

1 Thermodynamics

$$\xi \equiv \frac{n_i - n_{i0}}{\nu_i} = -\frac{X_A n_{A0}}{\nu_A} \quad \xi_e \equiv -\frac{X_e n_{A0}}{\nu_A} \quad \check{\xi} \equiv \frac{\xi}{V}$$

$$n_A = n_{A0} + \nu_A \xi = n_{A0}(1 - X) = 1 - \frac{n_i}{n_{i0}}$$

$$K_a = \prod_i a_i^{\nu_i} = e^{-\frac{\Delta G^\circ}{RT}} \quad K_P = \prod_i p_i^{\nu_i}$$

$$\frac{d \ln k}{dT} = \frac{E}{RT^2} \quad \frac{d \ln k}{dT^{-1}} = -\frac{E}{R} \quad \Delta_r G^\circ = \sum_i \nu_i \Delta G_i^\circ$$

$$\Delta G^\circ = \sum_i \nu_i \mu_i^\circ = -RT \sum_i \nu_i \ln a_i = -RT \ln K_a$$

$$\left[\frac{\partial(\Delta G^\circ/T)}{\partial T} \right]_P = -\frac{\Delta_r H}{T^2}$$

1.1 Properties of Gases

Ideal: $a_i = p_i$ Real: $a_i = \frac{f_i^*}{f_i^{\circ}}$

$$a_i = f_i = y_i f_i^* = y_i P \phi_i$$

$$K_a = K_p K_\phi \quad K_P = K_y P^\nu \quad \bar{v} = \sum_i \nu_i$$

1.2 Properties of Liquids

Ideal: $a_i = x_i$ Real: $a_i = x_i \gamma_i$

$$\left(\frac{d \ln K_a}{dT} \right)_P = \frac{\Delta H^\circ}{RT^2} \rightarrow \left[\frac{d \ln K_a}{d(1/T)} \right]_P = -\frac{\Delta H^\circ}{R}$$

2 Rate Law

$$k = A e^{-\frac{E_a}{RT}} \quad \check{r} = \check{r}_{fwd} - \check{r}_{rev} \quad \check{r} = k \prod_i c_i^{\alpha_i} \quad \bar{\alpha} = \sum_i \alpha_i$$

Order	Rate	Formula
0	$\check{r} = k$	$c_{A0} - c_A = kt$
1	$\check{r} = k c_A$	$\ln \frac{c_{A0}}{c_A} = kt$
2-I	$\check{r} = k c_A^2$	$c_A^{-1} - c_{A0}^{-1} = kt$
2-II	$\check{r} = k c_A c_B$	$\ln \frac{c_{A0}}{c_{B0}} + \ln \frac{c_B}{c_A} = (c_{A0} \nu_B - c_{B0} \nu_A) kt$
3-I	$\check{r} = k c_A^3$	$c_{A0}^{-2} - c_A^{-2} = 2 \nu_A kt$
3-II	$\check{r} = k c_A^2 c_B$	$c_A^{-1} - c_{A0}^{-1} + (c_{A0} - c_{B0} \frac{\nu_A}{\nu_B})^{-1} \ln \frac{c_B c_{A0}}{c_A c_{B0}}$ $= (c_{A0} \nu_B - c_{B0} \nu_A) kt$
3-III	$\check{r} = k c_A c_B c_Q$	$\nu_A (\nu_Q c_{B0} - \nu_A c_{Q0}) \ln \frac{c_A}{c_{A0}}$ $+ \nu_B (\nu_A c_{Q0} - \nu_Q c_{A0}) \ln \frac{c_B}{c_{B0}}$ $+ \nu_Q (\nu_B c_{A0} - \nu_A c_{B0}) \ln \frac{c_Q}{c_{Q0}}$ $= kt (\nu_A c_{B0} - \nu_B c_{A0}) (\nu_A c_{Q0} - \nu_Q c_{A0})$ $\times (\nu_Q c_{B0} - \nu_B c_{Q0})$
n	$\check{r} = k \prod_i c_i^{\alpha_i}$	$(c_A^{n-1})^{-1} - (c_{A0}^{n-1})^{-1} = (1-n) \nu_A kt$

$$\varepsilon_A \equiv \frac{V|_{X_A=1} - V|_{X_A=0}}{V|_{X_A=0}} = \frac{n_T|_{X_A=1} - n_T|_{X_A=0}}{n_T|_{X_A=0}}$$

$$\check{r} = [V_0(1 + \varepsilon_A X_A)]^{-1} \left(-\frac{n_{A0}}{\nu_A} \frac{dX_A}{dt} \right) = -\frac{c_{A0}}{1 + \varepsilon_A X_A} \frac{1}{\nu_A} \frac{dX_A}{dt}$$

$$\check{r} = \frac{1}{V} \frac{d\xi}{dt} = \frac{1}{V \nu_i} \frac{dn_i}{dt} = \frac{1}{\nu_i} \frac{dc_i}{dt} + \frac{c_i}{V \nu_i} \frac{dV}{dt}$$

$$N(t) = N_0 0.5^{t/\tau_{1/2}} = N_0 e^{-\frac{t}{\tau}} = N_0 e^{-\lambda t}$$

Order	0	1	2	3	n
$t_{1/2}$	$-\frac{c_{A0}}{2\nu_A k}$	$\frac{\ln 2}{k}$	$-\frac{1}{\nu_A k c_{A0}}$	$-\frac{3}{2\nu_A k c_{A0}^2}$	$\frac{2^{n-1} - 1}{(1-n)\nu_A k c_{A0}^{n-1}}$

3 Molecular Kinetics

$$\check{Z}_{AA} = 2(\rho_{N,A})^2 \sigma_A^2 \sqrt{\frac{\pi k_B T}{m}} \quad \check{Z}_{AB} = \rho_{N,A} \rho_{N,B} \pi \sigma_{AB}^2 \sqrt{\frac{8k_B T}{\pi \mu_{AB}}}$$

$$\sigma_{AB} = \frac{\sigma_A + \sigma_B}{2} \quad \mu_{AB} = \frac{\tilde{m}_A \tilde{m}_B}{\tilde{m}_A + \tilde{m}_B}$$

$$\check{r}_{AB} = \rho_s \check{Z}_{AB} e^{-\frac{E_a}{RT}} = k \rho_{N,A} \rho_{N,B}$$

4 Multiple Reactions

$$K_e = \frac{k_{fwd}}{k_{rev}} = \frac{c_{Be}}{c_{Ae}} \quad \check{r}_e = k_{fwd} - k_{rev} = 0$$

$$A \xrightleftharpoons[k_{rev}]{k_{fwd}} B : \check{r} = k_{fwd} c_A - k_{rev} c_B$$

$$-(k_{fwd} + k_{rev})t = \ln \frac{K_e c_A - c_B}{K_e c_{A0} - c_{B0}} = \ln \frac{\frac{c_{Be} c_A}{c_{Ae}} - c_B}{\frac{c_{Be} c_{A0}}{c_{Ae}} - c_{B0}}$$

$$A + B \xrightleftharpoons[k_{rev}]{k_{fwd}} R + S : \check{r} = k_{fwd} c_A c_B - k_{rev} c_R c_S$$

$$0 = K_e (c_{A0} - \check{\xi}_e)(c_{B0} - \check{\xi}_e) - (c_{R0} + \check{\xi}_e)(c_{S0} + \check{\xi}_e)$$

$$\zeta \equiv k_{fwd}(c_{Ae} + c_{Be}) + k_{rev}(c_{Re} + c_{Se})$$

$$\Delta \xi = \xi - \xi_e$$

$$t = \zeta^{-1} \ln \left(k_{fwd} - k_{rev} - \frac{\zeta}{\Delta \xi} \right)$$

$$A + B \xrightleftharpoons[k_{rev}]{k_{fwd}} R : \check{r} = k_{fwd} c_A c_B - k_{rev} c_R$$

$$\check{\xi}_e = \frac{K_e (c_{A0} + c_{B0}) + 1 + \sqrt{\zeta}}{2K_e}$$

$$\zeta \equiv K_e^2 (c_{A0} - c_{B0})^2 + 2K_e (c_{A0} + c_{B0} + 2c_{R0}) + 1$$

$$\Delta \xi = \xi - \xi_e$$

$$[k_{fwd}(c_{Ae} + c_{Be}) + k_{rev}]t = \ln \frac{\check{\xi}_e [K_e \Delta \xi - (K_e [c_{Ae} + c_{Be}] + 1)]}{\Delta \xi [K_e \check{\xi}_e + K_e (c_{Ae} + c_{Be}) + 1]}$$

$$A \xrightarrow[k_2]{k_1} R : \check{\xi}_1 = \frac{k_1 c_{A0}}{k_1 + k_2} (e^{-[k_1 + k_2]t}) \quad \check{\xi}_2 = \frac{k_2 c_{A0}}{k_1 + k_2} (e^{-[k_1 + k_2]t})$$

$$c_A = c_{A0} (e^{-[k_1 + k_2]t}) \quad \frac{c_R - c_{R0}}{c_T - c_{T0}} = \frac{k_1}{k_2}$$

5 Catalysis

$$K_{cat} = \frac{k_{ad}}{k_{de}} \quad \theta_v = 1 - \sum_i \theta_i$$

5.1 Single Species

$$\check{r}_{ad} = k_{ad} p_A (1 - \theta_A) \quad \check{r}_{de} = k_{de} \theta_A$$

$$\theta_A = \frac{k_{ad} p_A}{k_{de} + k_{ad} p_A} = \frac{K_{cat} p_A}{1 + K_{cat} p_A}$$

5.2 Multiple Species

$$A + B \xrightleftharpoons[k_{de}]{k_{ad}} R + S \quad \theta_v = 1 - \sum_i \theta_i$$

$$k_{ad,A} \theta_A \theta_B = k_{de,A} \theta_R \theta_S \quad \theta_A = \frac{\theta_R \theta_S}{K_{cat,A} \theta_B}$$

$$k_{ad,B} p_B \theta_v = k_{de,B} \theta_B \quad \theta_B = K_{cat,B} p_B \theta_v$$

$$\theta_R = K_{cat,R} p_R \theta_v \quad \theta_S = K_{cat,S} p_S \theta_v$$

$$\hat{r} = k_{ad,A} \left(p_A \theta_v - \frac{\theta_A}{K_{cat,A}} \right)$$

5.3 Dissociation Occurs on Adsorption

$$\check{r}_{ad} = k_{ad,A} p_A \theta_v^2 = k_{ad,A} (1 - \theta_A)^2 \quad \check{r}_{de} = k_{de,A} \theta_A^2$$

$$\theta_A = \frac{\sqrt{K_{cat,A} p_A}}{1 + \sqrt{K_{cat,A} p_A}}$$

Only A dissociates: $\theta_A = \frac{\sqrt{K_{cat,A} p_A}}{1 + \sqrt{K_{cat,A} p_A} + K_{cat,B} p_B + K_{cat,C} p_C}$

6 Reactor Design

6.1 Batch Reactor

$$t = c_{A0} \int_0^{X_A} \frac{dX_A}{-\check{r}_A} = -\int_{c_{A0}}^{c_A} \frac{dc_A}{-\check{r}_A}$$

$$t = n_{A0} \int_0^{X_A} \frac{dX_A}{-\check{r}_A V_0 (1 + \varepsilon_A X_A)} = c_{A0} \int_0^{X_A} \frac{dX_A}{-\check{r}_A (1 + \varepsilon_A X_A)}$$

$$c_A = c_{A0} (1 - X_A) \quad c_Z = c_{Z0} + c_{A0} X_A$$

6.2 Plug Flow Reactor

$$\frac{V}{F_{A0}} = \int_{X_{A,in}}^{X_{A,out}} \frac{dX_A}{-\check{r}_A} \quad \tau = \frac{V}{V_0} = c_{A0} \int_{X_{A,in}}^{X_{A,out}} \frac{dX_A}{-\check{r}_A}$$

$$\{\varepsilon = 0\} : \tau = -\int_{c_{A,in}}^{c_{A,out}} \frac{dc_A}{-\check{r}_A}$$

Gas: $c_A = c_{A0} \frac{1 - X_A}{1 + \varepsilon_A X_A}$

$$t_m = \int_{X_{A,in}}^{X_{A,out}} \frac{F_{A0} dX_A}{-\check{r}_A V_0 (1 + \varepsilon_A X_A)} = c_{A0} \int_{X_{A,in}}^{X_{A,out}} \frac{dX_A}{-\check{r}_A (1 + \varepsilon_A X_A)}$$

6.3 CSTR

$$\frac{V}{F_{A0}} = \frac{X_{A,out} - X_{A,in}}{-\tilde{r}_{A,out}}$$

$$\tau = \frac{c_{A0}}{-\tilde{r}_{A,out}} (X_{A,out} - X_{A,in}) = \frac{c_{A0}}{-\tilde{r}_{A,out}} \int_{X_{A,in}}^{X_{A,out}} dX_A$$

$$\tau = \frac{1}{-\tilde{r}_{A,out}} (c_{A,out} - c_{A,in}) = \frac{1}{-\tilde{r}_{A,out}} \int_{c_{A,in}}^{c_{A,out}} dc_A$$

6.4 PFR Recycle Reactor

$$\frac{V}{F_{A0}} = (R+1) \int_{X_{A,PFR\ in}}^{X_{A,PFR\ out}} \frac{dX_A}{-\tilde{r}_A} \quad X_{A,PFR\ in} = \frac{R}{R+1} X_{A,PFR\ out}$$

$$R \equiv \frac{\text{volume of fluid returned}}{\text{volume of fluid leaving in net product}}$$

7 Temperature and Energy Effects

$$\text{Batch: } \dot{Q} = \tilde{r}V \Delta_r H + \sum (n_i \bar{C}_{P,i} \frac{dT}{dt}) \quad T = T_0 + \frac{\Delta_r H(T_0) n_{A0} X_A}{\nu_A \sum (n_i \bar{C}_{P,i})}$$

$$\text{CSTR: } \dot{Q} = \frac{F_{A0}(X_{A,out} - X_{A,in})}{-\nu_A} \Delta_r H(T_0) + \sum \left(F_i \int_{T_0}^{T_{out}} \bar{C}_{P,i} dT \right)$$

$$\text{Tubular reactor: } \int_{X_{A,in}}^{X_{A,out}} U \Delta T \frac{A}{\emptyset} F_{A0} \frac{dX_A}{-\tilde{r}_A} = \sum \left(F_i \int_{T_0}^T \bar{C}_{P,i} dT \right) - \frac{F_{A0} \Delta_r H(T_0)}{\nu_A} (X_{A,out} - X_{A,in})$$

8 Deviation from Ideal Flow

$$t_m = t = \int_{t=0}^{t=\infty} t \left(\frac{dF(t)}{dt} \right) dt$$

References

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